



TEEG -Turbomachinery Energy Environment Group

Bioenergy integrated systems and Small Plants Research activity

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Outline of presentation:

- ✓ *The New Center For Renewable Energy in Florence & the active projects*
- ✓ *Small Scale power plant activity & testing (Falascaia)*
- ✓ *Micro Cogeneration System: preliminar study (Sambuca)*
- ✓ *Feasibility study of small-micro integrated plants*
- ✓ *Numerical modelling & simulation of critical equipments*
- ✓ *Regional Biomass Exploitation: technical & Economical evaluation*

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C.R.E.A.R.

Centro di Ricerca sulle Energie Alternative e Rinnovabili

Objective: *Coordinate and organize synergy research activity based on multidisciplinary of renewable Energy. Increase competition capability of Research groups.*

Activity: *Set up a laboratory to test and develop small power plants for distributed energy production; based on up to date technology for biomass use, and other renewable source (wind, Geo, Solar..). Research project coordination.*

Members: *Dip. Energetica+3 Dip. Agricultural+Dip. Chemistry,Dip. Geology*

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A number of completed and on-going biomass projects. Among others:

- **BIOSIT** (GIS-Biomass resource assessment) – Life Programme
- **COMBIO** (Pyrolysis Oil – Emulsions for Heating) – 5PQ
- **OPRODES** (Renewable Energy Desalination) – 5PQ
- **TOSCANAPA** (Impianto macerazione canapa) – R.T.Progr.ITT
- **ENVIRONMENTAL IMPACT ASSESSMENT** (biomass, wind)
- **CROPENERGY** (Bioenergy production from Energy Crops) – 6PQ-STREP
- **BIOCHAIN** (Development of a bioenergy chain on the Amiata mountain)
- **BIO-FOOD-ENERGY FARM** (Demonstration project for the development of integrated food-energy farms)
- Other activities on **PELLETISATION TECHNOLOGIES**, pre-treatment, etc.

.. moreover ...

➤ **IMES** – EU-USA International Master Course on Bioenergy and Environment (Univ.di Firenze, Univ.di Aston, Univ.di Lisbona – Baylor, Arizona e Texas Univ.s)

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✓ Experimental tests on the Falascaia Plant (Lucca-Tuscany)

The Falascaia plant has been designed for the power generation from urban wastes and biomass through a steam cycle

The tests have been performed while burning chipped pine and latifoglie triturate

Main Components:

- ⊗ 2 Bubbling Fluid Bed reactors of 12 MWt each
- ⊗ Steam turbine (Ansaldo), coupled with a generator ~ 5 MWe
- ⊗ Emission treatment of the exhaust: SNCR, cyclons, filter fly ash, scrubber



Experimental tests on the Falascaia Plant (Lucca-Tuscany) **Plant Analysis: Objectives and Methodology**

Objectives

- ▣ Recommendations for an optimal plant regulation
- ▣ Methodology of the teoretical-experimental tests

Analysis methodology

- ▣ Modelling of the plant and definition of the plant variables
- ▣ Performance variables set
- ▣ Experimental data acquisition
- ▣ Post-processing of data
- ▣ Regulation variables set
- ▣ Results and sensitivity analysis





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AIR-PHOTOGRAPH of the PLANT



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PLANT ANALYSIS

■ Modelling of the plant and definition of the plant variables

In the Falascaia plant, many variables are continuously monitored (temperatures, pressures, fluxes, et.) and measured. Others can be computed from the monitored ones, through the model developed:

measured variables + analytically computed variables



We determined the variables describing the performances and the ones that can be set to optimize the performance, i.e.:

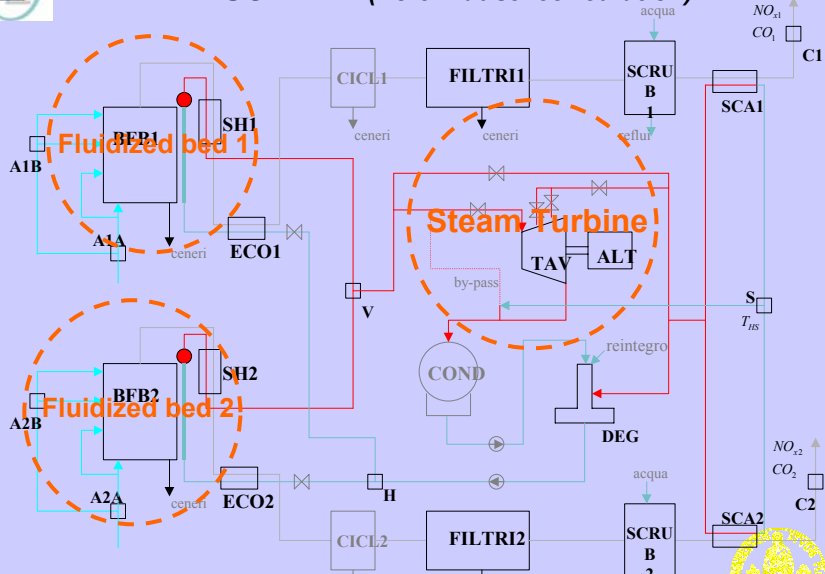
performance variables + Control variables

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PLANT SCHEME (no exhaust recirculation)



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PLANT ANALYSIS

Performance variables set

The monitoring operations and the regulation are concentrated on to the fluidized beds; the power generation isle can be regulated only through steam spillages. Thus, both the performances and the controll variables concern the reactors

Performance variables

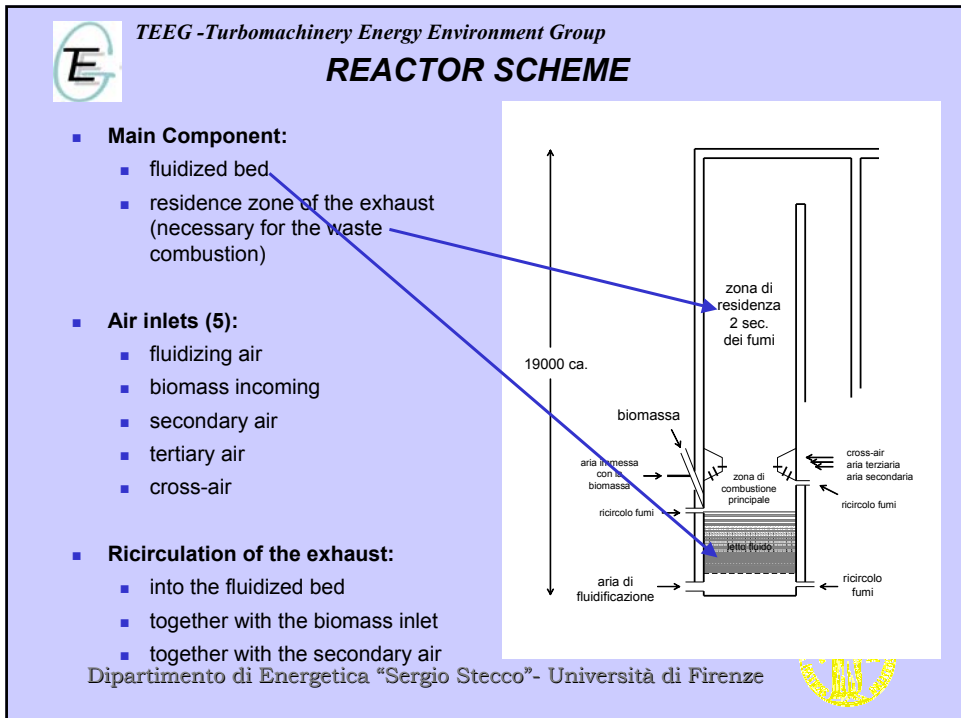
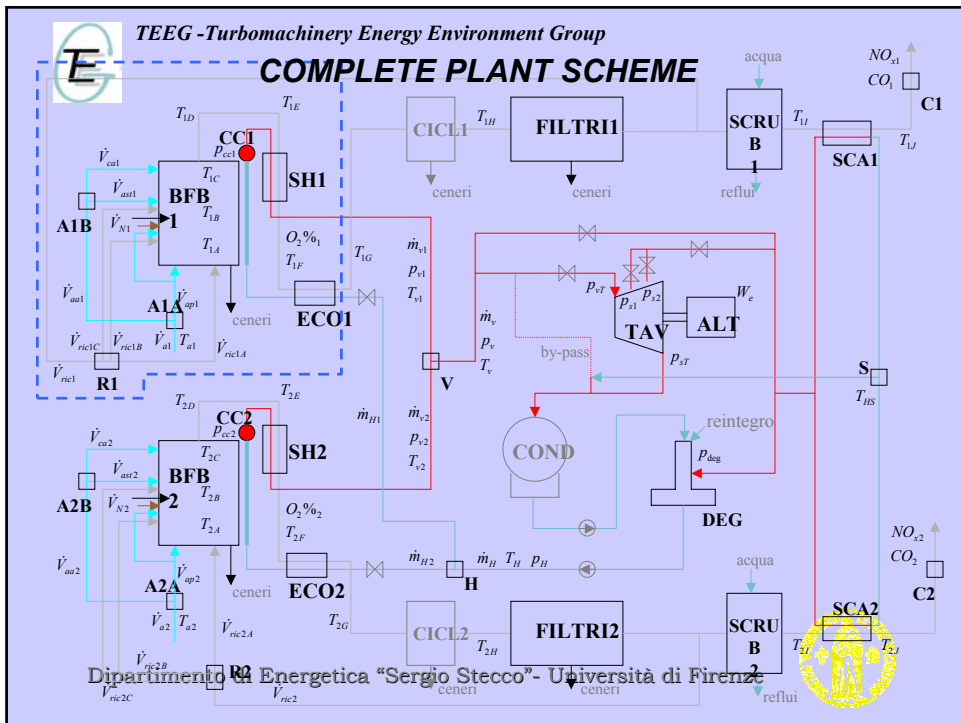
η_{combust} , thermal duty, emissions (CO, NO_x, organic contaminants), NH₃ consumption

The controll variables are determined based on the plant model and on the sensitivity analysis. They are chosen among the measured and the analytically computed variables

plant scheme: measured variables

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EXPERIMENTAL TESTS AND ANALYSIS

Experimental data acquisition :

- steady working conditions
- large range of thermal duty

→ Data corresponding to 23 performance variable monitoring have been collected in different working conditions and with different biomass humidity

Post-processing of data to determine the variables which are not measured



Controll variables set choice

Controll variables:

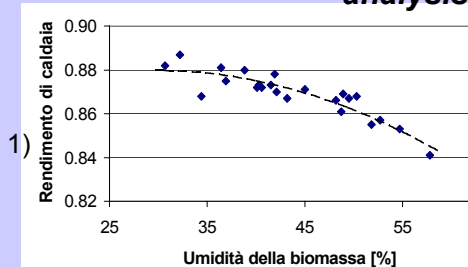
1) biomass humidity, 2) air excess, 3) temperature of the main combustion zone, 4) total flux of the exhaust recirculation

Results and sensitivity analysis

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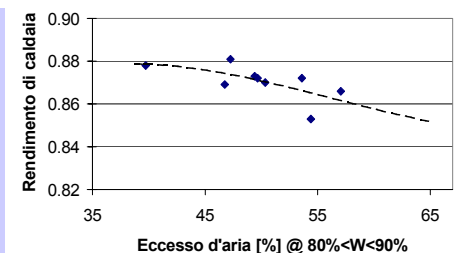


EXPERIMENTAL RESULTS: sensitivity analysis



← Efficiency of the reactor decreasing with biomass humidity

Efficiency of the reactor decreasing with air excess → 2)



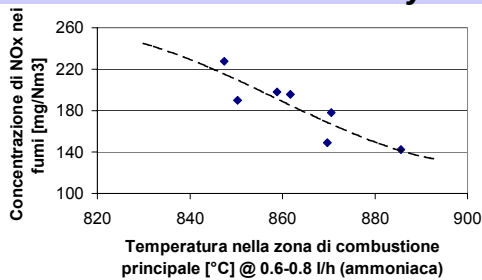
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EXPERIMENTAL RESULTS: sensitivity analysis

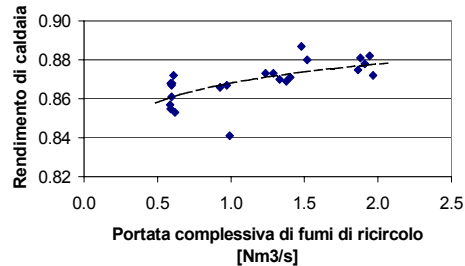
3)



← NOx emission decreasing with temperature

Efficiency of the reactor increasing with the exhaust recirculation flow rate

4)



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CONCLUDING REMARKS

Recommendations for an optimal plant regulation

The optimal values of the following parameters have been determined :

- Biomass humidit, to increase the efficiency
- Air excess (measured through the O₂ content monitored in the moist exhaust)
- Minimum value of the temperature in the main combustion zone, to limit the NO_x formation, thus the NH₃ employment
- Maximum value of the NH₃ rate, less than 2 l/h, to take the NO_x under the low limit
- Recirculation flow of the exhaust into the fluidized bed
- Minimum value of the fluidized bed temperature, to increase the efficiency
- No recommendations have been considered for CO, since the emission are low





✓ **Micro Cogeneration System: preliminar study** **(Sambuca- Tuscany)**

BIOMASS MICRO COGENERATION SYSTEM IN AN INDUSTRIAL AREA OF TUSCANY CHIANTI HILLS :

❖ What chances to instal & operate a **300 – 600 kWe micro cogeneration system** in an existing industrial park of Tuscany Chianti hills ?

THERMODYNAMIC AND COSTS ANALYSIS

❖ The study is based on the analysis of the local agricultural and industrial **wastes potential within an of up to 5 kilometres transport distance**, which defines the power plant size

❖ The **optimisation of heat recovery, related to the local utilities**, was a further essential aspect which addressed the power cycle layout. The option of **providing heat for a local system of waste water treatment** was also considered and evaluated

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THERMODYNAMIC AND COSTS ANALYSIS

❖ The possible options of electrical generator drivers such as **internal combustion engine** and Organic Rankine Cycle (**ORC**) were evaluated and compared

❖ The **thermodynamic and costs analysis** was carried out referring to **four possible scenarios**, defined by the **availability of primary biomass fuel**. A sensitivity analysis to the variable cost of fuel was also performed in terms of payback period and Net Present Value

❖ The study lead to the **conclusion** that **the investigated area might be an interesting site for installing a biomass micro cogeneration power plant**, with both energy and economic profitability for the local companies, especially if coupled with the water treatment system

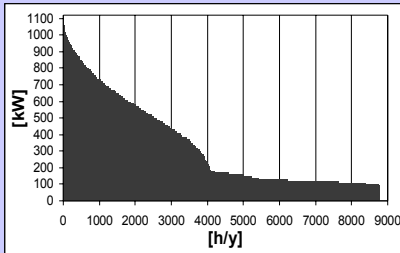
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Users CHP demand and technical solutions

The Sambuca industrial park is a local system of SMEs (Small and Medium Enterprises) located in a rather flat and narrow Chianti valley on the sides of the Pesa river, nearby Florence-Siena highway



Heat duration curve in the Sambuca industrial park

HP1	Industrial and agricultural (caseA) waste wood	2655t/y
HP 2	Industrial and agricultural (caseB) waste wood	5400 t/y
HP 3	Industrial and from selective collection waste wood	2200 t/y
HP 4	Agricultural (case A) and from selective collection waste wood	3255 t/y

Biomass availability in the four possible operating conditions

Main goal of this work is to show the economic feasibility of the proposed project
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Down-draft gasifier coupled to a gas engine for CHP production

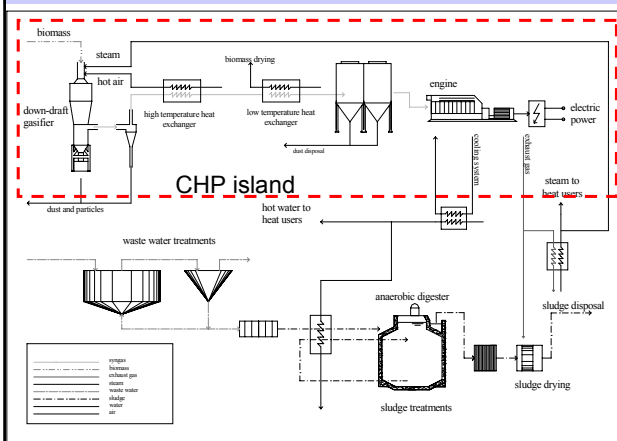


Table 2 - CHP thermodynamic data

	HP 1	HP 2	HP 3	HP 4
w_{exp} [hrs/y]	7.500	7.500	7.500	7.500
W_{gr} [kWe]	317	679	313	431
η_{el} [%]	23,3	23,3	20	20
η_{th}	31%	29%	35%	32%
$\eta_{th,exch}$ [%]	15	14	16,8	15,6
$\eta_{th,cool}$ [%]	19,5	18	21,6	20,1
$W_{th,exch}$ [kWt]	1.504	3.005	1.321	1.844
$W_{th,cool}$ [kWt]	203	377	202	258
$W_{th,exch}$ [kWt]	264	483	260	333
$W_{th,engine}$ [kWt]	467	859	462	591
$W_{th,max,used}$ [kWt]	409	681	413	519
$W_{st, gasifier}$ [kWt]	38	178	49	72
E_{el} [MWe/y]	2.381	5.095	2.350	3.230
$E_{th, fuel}$ [MWh/y]	11.283	22.534	9.910	13.833
E_{th} [MWh/y]	3.067	5.110	3.101	3.896
$E_{th, used}$ [MWh/y]	1.915	2.424	1.928	2.188
η_1 [%]	38	33	43	39
LHV _{bio} [kJ/kg]	14923	14628	15885	14912
LHV _{sp} [kJ/kg]	4622	4493	5459	4982
W_{bio} [%]	15,5	16,2	13,6	15,9
m_{bio} [kg/s]	0.10	0.20	0,08	0.12





CHP plant based on ORC SYSTEM

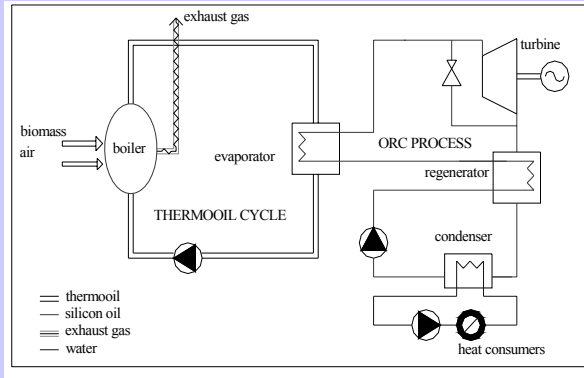


Table 3 – Main operating data of ORC in the two supposed case studies

	HP α	HP β
Biomass flow [t/y]	6200	8300
Biomass LHV [kJ/kg]	15221	15317
Electric efficiency [%]	17	17
Boiler efficiency [%]	75	75
Electric power [kWe]	446	600
Thermal power [kWh]	2025	2800
Working hours [h/y]	7500	7500



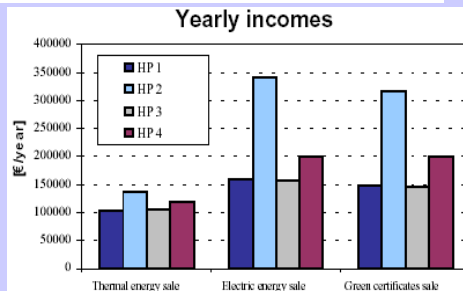
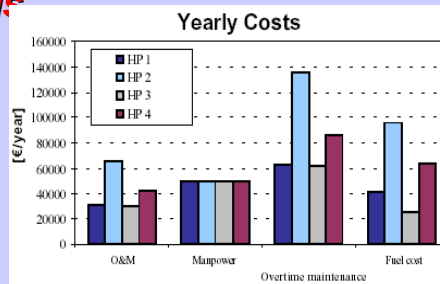
Economic analysis

Investment costs of the proposed CHP in the four possible considered scenarios

CHP investment costs	HP 1	HP 2	HP 3	HP 4
Powerplant components (gasifier, cogenerator, heat exchangers, syngas cleanup system, generator, control system) [k€]	713.3	1526.0	703.9	967.5
Land purchasing [€]	60	60	60	60
Buildings, auxiliaries, biomass fuel storage [k€]	70	70	70	70
Heat distribution network [k€]	65.43	109.02	66.16	83.12
Total [k€]	908.7	1765.1	900.0	1180.6
Overtime after which additional maintenance costs are required [khrs]	40	40	40	40
CHP life [khrs]	112.5	112.5	112.5	112.5
Unit biofuel cost [€/ton]	15.5	17.8	11.4	19.6
Incomes taxes [%]	40	40	40	40
CHP lifetime [y]	15	15	15	15
Discount rate [%]	12	12	12	12
Inflation rate [%]	2.5	2.5	2.5	2.5

Financial parameters of the six possible CHP options

	NPV [k€]	PBT [y]	IRR [%]	Incentive 25%		
				NPV [k€]	PBT [y]	IRR [%]
HP1	373.6	6-7	20.1	600.8	4-5	28.7
HP2	770.1	6-7	20.6	1213.8	4-5	29.5
HP3	446.2	6-7	21.6	671.2	4-5	30.4
HP4	495.8	6-7	20.3	791.0	4-5	29.0
HPα	763.2	6-7	18.6	1035.0	4-5	26.7
HPβ	705.7	6-7	20.8	1096.2	4-5	29.5





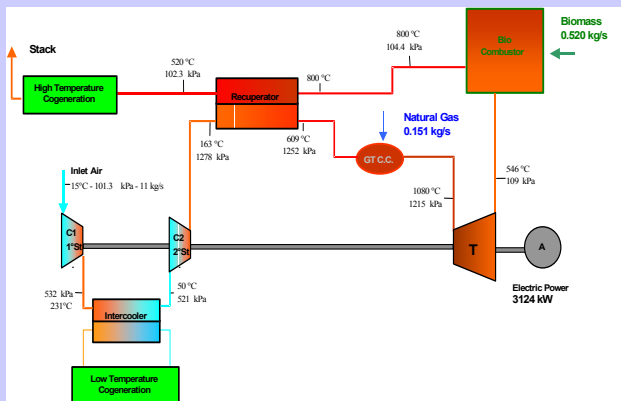
✓ Feasibility study of small-micro integrated plants

- ❖ External Fired Gas Turbine Power Plant Fed by Solid Fuel
- ❖ Integrated micro-turbine & gasifier with FC & renewable energy supply



External Fired Gas Turbine Power Plant Fed by Solid Fuel

DCGT - Dual Combustor Gas Turbine



Technical Features

- Gas Turbine Power Plant

- Dual Combustion:

Internal Combustion of natural gas (or biofuel-ethanol) in GT comb. chamber

External Combustion of solid biomass in grate furnace or BFB at atm P

- Intercooling

Performances

- Net Electric Power 3124 kW
- Net Efficiency 25.6 %
- Energy ratio Biomass/Natural gas 0.83
- Cost per kWh of net electric Power 0.057€

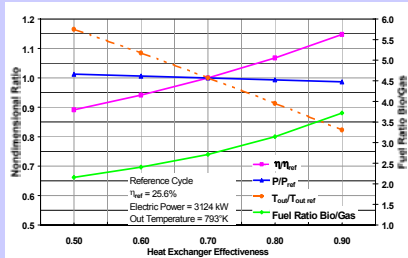




Advantages & Peculiarities

- Direct combustion of solid state biomass at atmospheric pressure
- Smaller size of the plant in comparison with a steam power plant
- Satisfactory Performances ($\eta = 25.6\%$)
- Wide cogeneration possibility ($T_{low} = 231^\circ\text{C}$; $T_{high} = 520^\circ\text{C}$)
- Competitive cost investment

Heat Exchanger Effectiveness Sensitivity analysis :



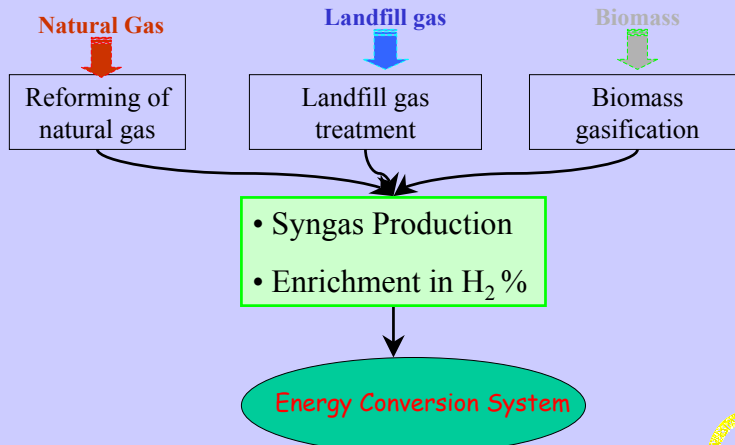
Key Points

- Combustion Systems
- Heat Exchanger Technology
- Automatic Biomass Supply and Plant Control

$$\varepsilon = \frac{T_{out-COLD} - T_{in-COLD}}{T_{in-HOT} - T_{in-COLD}}$$



Integrated system for production and energy conversion of Renewable sources





Energy Conversion System

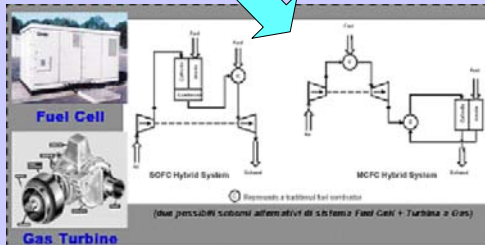


Energy Conversion System

Reciprocal
Engine (CHP)

Micro GT / Fuel
Cell integrated
system

R&D on Fuel
Cell



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✓ *Numerical modelling & simulation
of critical equipments*

❖ *CFD of GT Combustion Chamber*

Aerodynamic simulation of the liner: study of the swirler angle influence

❖ *Biomass gasification kinetics model*

A two-phase one-dimensional model

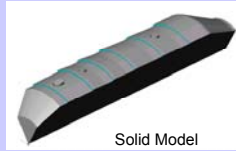
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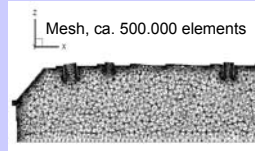


CFD of GT Combustion Chamber

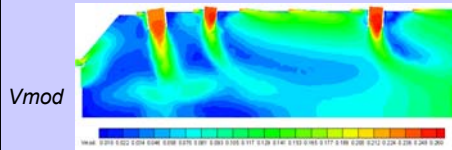
Aerodynamic simulation of the liner: study of the swirler angle influence



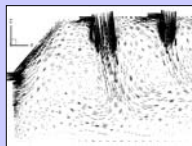
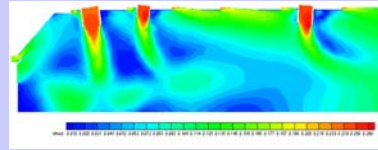
Solid Model



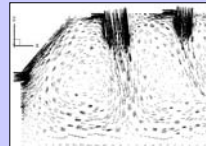
Mesh, ca. 500.000 elements



Vmod



ϑ flusso 30°



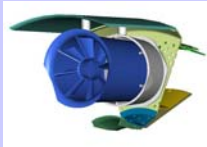
ϑ flusso 45°

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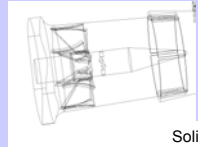


CFD of GT Combustion Chamber

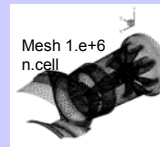
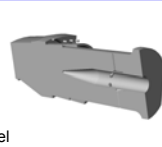
Detailed simulation: air-fuel mixing in premixing duct



Geometry

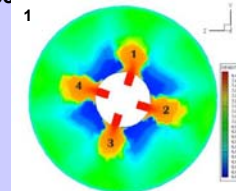
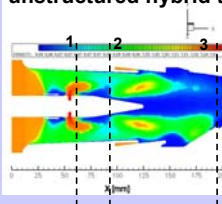


Solid model

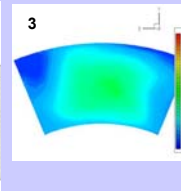
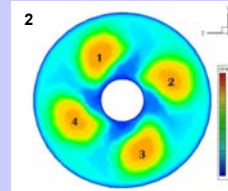


Mesh 1.e+6 n.cell

Computation by the CFD code Hybflow: 3-D "Full-Navier Stokes" finite volume code of unstructured hybrid type in house developed



X=64



- Air/fuel Mixing evaluation: *std (fuel conc.)*
- Aerodynamic performances

Study of modifications
 Tuning of simplified design model

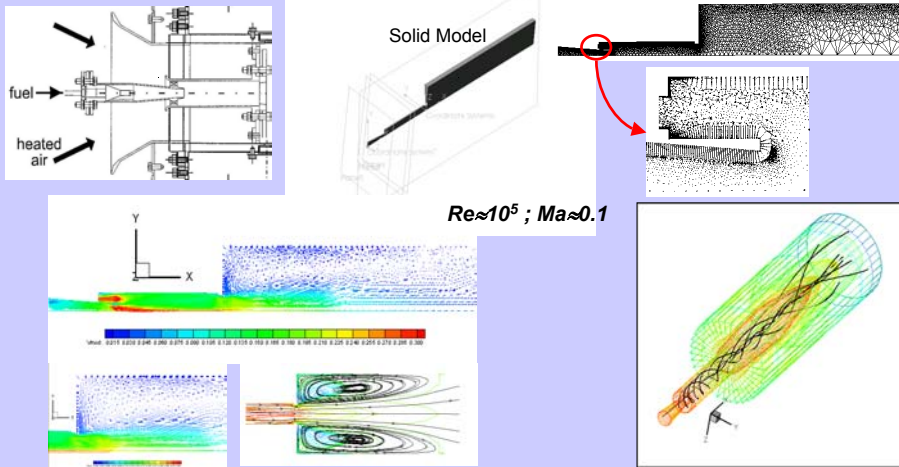
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CFD of Lean Premixed Prevaporised (LPP) injection system Detailed simulation: air-fuel mixing in premixing duct



Streamlines e pressione statica at the combustion volume inlet
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❖ A two-phase one-dimensional biomass gasification kinetics model

Operating environment: bubbling fluidized beds

Model type: one-dimensional

Calculated parameters

- temperature along the reactor axis
- concentration gradients along the reactor axis
- considers two phases, a bubble and a dense phase and accounts reaction kinetics in the dense phase
- mass transfer between the two phases and a quantitative estimation of local bubble and particle properties

Model's optimisation parameters

- ER (Equivalence Ratio)
- Reactor pressure
- Bed height
- Gas velocity

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Mathematical one-dimensional model for the fluidized bed reactor

Double – phase model

dense phase (gas plus solid particles)
 bubble phase (mainly gaseous with much lower solid matter)

- two-phase reactor modeled as the sum of several elemental reactors of dz thickness
- Differential equations are solved vs. temperature and syngas composition, along the gasifier axis, for both dense and bubble phases

The gas flow entering the reactor at v_0 speed is splitted into two phases: the dense phase, (minimum fluidization velocity v_{mf}), and the bubble phase, (the velocity is $v_0 - v_{mf}$)

overall mass balance for bubble and dense phases

$$(v_0 - v_{mf}) \frac{dC_b}{dz} + v_{mf} \frac{dC_d}{dz} + r(1 - \epsilon_b) = 0$$

Molar concentration of the i^{th} component into the two phases

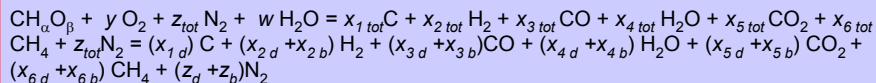
$$C_{id} = \frac{x_{id} \cdot n_b}{(1 - \epsilon_b) \cdot V_{tot}} \quad \text{Dense Bubble} \quad C_{ib} = \frac{x_{ib} \cdot n_b}{\epsilon_b \cdot V_{tot}}$$

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Evaluation of the overall reaction kinetics

From one mole of a generic biomass $\text{CH}_\alpha\text{O}_\beta$ (d="dense", b="bubble", tot="dense+bubble", x_i ="ith" specie concentration in gas):



Chemical gasification reactions considered in the mathematical model:

- $\text{C} + \text{CO}_2 = 2\text{CO}$
- $\text{C} + \text{H}_2\text{O} = \text{H}_2 + \text{CO}$
- $\text{C} + 2\text{H}_2 = \text{CH}_4$
- $\text{H}_2\text{O} + \text{CH}_4 = \text{CO} + 3\text{H}_2$

Serial effects of chemical kinetics and mass transfer limit the gasification speed: Then, the rate of the i^{th} chemical specie follows (electrical model analogy):

$$v_i = \frac{v_{it} v_{ikin}}{v_{it} + v_{ikin}}$$

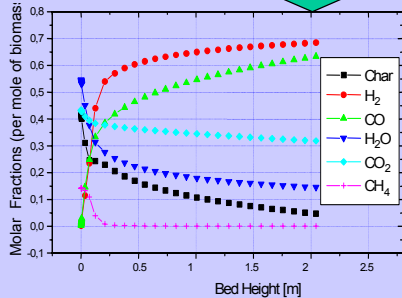
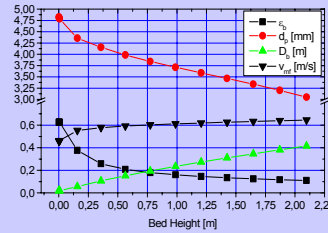
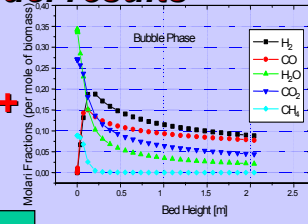
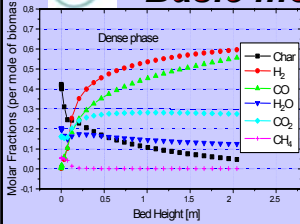
The temperature has been evaluated by a thermal balance along each of the elemental reactors into which the fluidized bed has been divided (time interval $t_{j+1} - t_j$):

$$\sum_{i_{tot}=1}^{ns} x_{i_{tot}}(t_j) h_{i_{tot}} + \sum_{i_{tot}=1}^{ns} x_{i_{tot}}(t_j) h_{f_{i_{tot}}} = \sum_{i_{tot}=1}^{ns} x_{i_{tot}}(t_{j+1}) h_{i_{tot}} + \sum_{i_{tot}=1}^{ns} x_{i_{tot}}(t_{j+1}) h_{f_{i_{tot}}} + q_i(t_j)$$



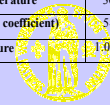


Basic model results



Biomass composition (sawdust)	velocity $v_{0.59}$	λ	3
Humidity (dry basis)	10 %	Primary fragmentation factor n_1	1.1
ER	0.33	Secondary fragmentation factor n_2	1.8
Oxidizer	air	Oxidizer inlet speed v_o	1 m/s
Bed Height	2.1 m	Reactor wall thickness	0.25 m
Bed diameter d_r	1.30 m	External convection	10 W/m ² K
Initial char particles diameter	5 mm	Wall conductivity	0.1 W/m K
Char density	1500 kg/m ³	External temperature	30 °C
Inert particles diameter	800 μ m	k_{er} (elutriation coefficient)	$5 \cdot 10^{-6}$
Inert particles density	2600 kg/m ³	Gasifier pressure	1.013 bar

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Regional Biomass Exploitation:

technical & Economical evaluation

BIOSIT

GIS-based planning tool for greenhouse gases emission reduction through biomass exploitation

Supported by the European Commission LIFE-Environment demonstration projects



PARTNERSHIP

DE - Dipartimento di Energetica "S.Stecco" Florence University *coordinator*

DEART - Dipartimento Economico Agrario Risorse Territoriali Florence University

ETA - Energy-Trasports-Agriculture, Company

Dipartimento di Energetica "Sergio Stecco" - Università di Firenze





BIOSIT

GIS-based planning tool for greenhouse gases emission reduction through biomass exploitation



Objective of the project: to develop an innovative tool, based onto the Territorial Information System, to support the biomass management for energy production in Tuscany.

The specific objectives are the following:

- 1) *Promotion and sustainable development of biomass to energy plants;*
- 2) *Reduction of atmospheric pollutants emission and CO emission;*
- 4) *Valorisation of the territory, recovery of marginal areas;*
- 5) *Improved management of forestry and agricultural land*
- 6) *Integration between rural and urban areas*

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Action 1: GIS-based analysis of biomass production in Tuscany

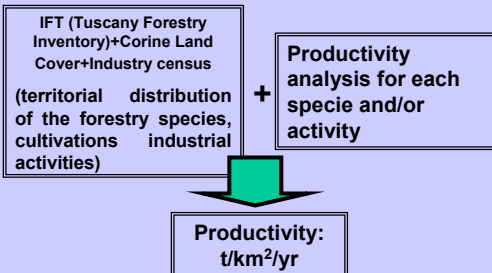
Biomass-to-energy resources typologies

Present resources

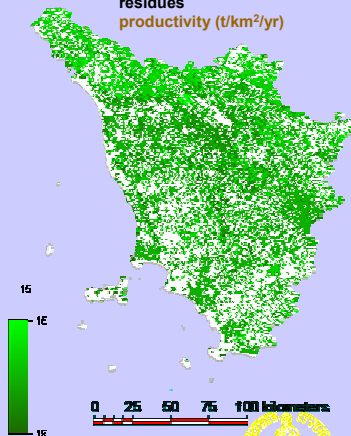
- Forestry residues (from felling operations)
- Wood industry residues
- Agricultural residues: fruit trees pruning and herbaceous residues from cereal cultivations

Potential resources

- Short Rotation Forestry (SRF)
- Energy Crops (herbaceous)



Example:
cereal residues and forestry residues
productivity (t/km²/yr)



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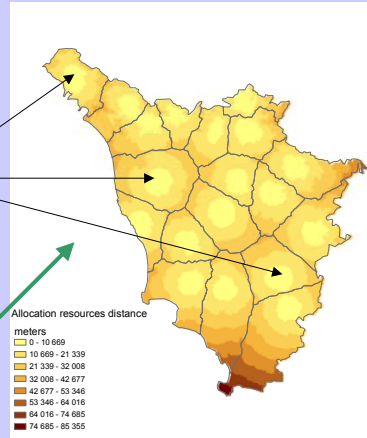


Action 2: Design and implementation of a computational algorithm of the biomass total cost (from the collection to the plant); supply basins definition

- 1) GIS implementation of the computational algorithm of the total costs: production, collection, stocking and transport to the stockpile centre
- 2) 19 stockpiling center have been identified, with strategic characteristics (existing infrastructures, industrial areas)
- 3) Transport costs optimization

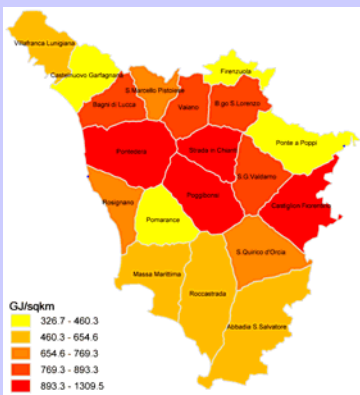


Optimal surface extension of the 19 supply basins



Action 3: GIS-based evaluation of the energy potential and the optimal plant distribution

Example:
energy potential of agricultural
and forestry residues
GJ/km²/yr



SUPPLY BASINS	INSTALLABLE POWER (MWE)
Villafranca Lunigiana	6.55
Firenzuola	2.0
Castelnuovo Garfagnana	4.675
S.Marcello Pistoiese	4.15
Bagni di Lucca	7.775
B.go S.Lorenzo	6.45
Vaiano	3.77
Ponte a Poppi	5.26
Strada in Chianti	11.85
Pontedera	14.8
S.G.Valdarno	7.475
Poggibonsi	10.03
Pomarance	4.30
Castiglion Fiorentino	10.7
Rosignano	5.25
S.Quirico d'Orcia	8.4
Massa Marittima	4.77
Roccastrada	8.3
Abbadia S.Salvatore	9.75
TOTAL	136.255





Action 4: Evaluation of the environmental and social impact of the bioenergy sector

Example:
CO2 avoided through the energy conversion of biomass from agricultural residues instead of fossil fuels (t/ha/yr)

Employment impact (# of workers) for biomass collection and transport in the bioenergy sector

